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September 2003 (19.09.03)
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<u>Priority date</u>	Priority application No.	Country or regional Office or PCT receiving Office	<u>Date of receipt</u> of priority document
21 Sept 2002 (21.09.02)	0221995.4	GB	06 Nove 2003 (06.11.03)

The International Bureau of WIPO 34, chemin des Colombettes 1211 Geneva 20, Switzerland

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5.	Name of your agent (if you have one)	W. P. Thompson & Co.	
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Description

8

Claims

Abstract

Drawing(s)

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Priority documents

Translations of priority documents

Statement of inventorship and right to grant of a patent (Patents Form 7/77)

Request for preliminary examination and search (Patents Form 9/77)

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IMPROVEMENTS IN ELECTROMECHANICAL TRANSDUCERS

This invention relates generally to electromechanical particularly concerned with is and transducers, 5 electrodynamic loudspeakers.

Electrodynamic loudspeakers typically use permanent magnets within a magnetic circuit of ferromagnetic material to create magnetic flux in an air gap within which a voice coil is displaceable. The magnetic circuit directs the flux produced by the permanent magnet into the air gap. current flows through the voice coil, the magnetic flux in The voice coil receives signals the air gap is constant. which produce a current in the coil in a direction which is substantially perpendicular to the direction of the lines of 15 magnetic flux produced by the permanent magnet. The coil is connected mechanically to a diaphragm which is driven by the axial motion of the coil produced by the motor force on the coil.

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Various types of distortion can arise in the translation 20 of a given electrical signal from an amplifier into the sound heard by a listener. A particular problem arises in relation to second harmonic and third harmonic distortion.

A further factor which is relevant to the design of loudspeakers is the length of the voice coil or voice coils in relation to the length of the air gap within which the 25 coil or coils move. In most loudspeaker designs the length of the coil is more than the length of the air gap and the axial motion of the coil is substantially dependent on the length of the coil, so that the voice coil does not move

beyond the region in which the flux density is substantially constant and perpendicular to the coil. In the case of a short or "underhung" coil magnetic modulation distortion can occur which affects the linearity of response of the loudspeaker. The magnetic field which is generated by the voice coil modulates the field in the air gap which interacts with the current voice coil to generate the driving force. In the air gap there are two magnetic fields, one generated by the voice coil and one generated by the permanent magnet.

These fields are not superimposed but are added to each other. This causes distortion, particularly second harmonic and third harmonic distortion, because the driving force will vary depending upon the incoming signal to the voice coil. This is particularly so at low frequencies.

Attempts have been made to solve these problems by using a short voice coil within a long air gap. However, although this is a customary design, it has only limited effectiveness.

It is also known to try to overcome this problem by creating eddy currents in the magnetic circuit to produce a magnetic field which opposes the magnetic field generated by the voice coil. This can help to reduce the variations in magnetic flux to some extent.

It is also known to stabilise the magnetic flux profile

25 by setting conductive rings into the pole piece. With the

correct length of coil this does give some improvement in

reducing distortion. However, because the flux through the

voice coil and the flux within the magnetic circuit is not

ideal, and because of the resistance and skin effects of the

conductive rings, which limits the current, these flux stabilization measures become ineffective at low frequencies.

International patent application WO91/05447 describes an electrodynamic speaker in which a shorted turn is positioned in the air gap to reduce the inductance that the loudspeaker presents as a load to a driving source and to increase the fidelity of reproduction of an input signal.

International patent application WO/89/02501 describes a magnetic circuit for an electromechanical transducer, such as a loudspeaker, in which compensating coils or compensating conductors are provided within grooves formed in the surface the pole pieces of the magnetic circuit. compensating coils or conductors are supplied with a current corresponding to the signal current, in order to produce an 15 opposing magnetic field to that produced by the voice coil.

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None of these known designs and structures is able significantly to reduce second harmonic and third harmonic distortion at low frequencies.

It is an object of the present invention to provide an electromechanical transducer, particularly an electrodynamic 20 loudspeaker, in which second harmonic and third harmonic distortion is significantly reduced, especially at low to mid-range frequencies, i.e. up to about 150 Hz.

It is a further object of the present invention to provide a loudspeaker driver which has exceptionally high linearity.

The present invention is based upon the recognition that the path of the magnetic flux from the voice coil through the pole pieces is not the same as the path of the magnetic flux

through the pole pieces. permanent magnet the in accordance with the invention, Consequently, permeability of the path of the magnetic flux from the voice coil is decreased, by decreasing the permeability of the 5 magnetic circuit. This decrease in the permeability of the magnetic circuit is achieved by splitting or dividing the magnetic circuit to make it a multi-pole circuit. achieved by introducing at least one separation into the magnetic circuit, thereby to create at least two, preferably three or more poles.

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be magnetic circuit of the division This accomplished by the use of air gaps and/or rings conductive or non-conductive material within the magnetic circuit. In this way one can create two or more poles, thus 15 decreasing the permeability of the magnetic circuit and enabling the achievement of an ultra-linear driver.

The present invention is not limited to the use of a single voice coil within the air gap of the loudspeaker. The invention is also appropriate to embodiments which use two 20 voice coils within the air gap.

A further advantage of the present invention is that the choice of coil length and gap length is less critical. can even use a long coil within a short gap, although there will be some flux modulations with such a configuration.

that the invention may be more fully In order understood, a number of embodiments in accordance with the invention will now be described by way of example and with reference to the accompanying drawings. In the drawings:

Fig. 1 is a schematic diagram showing a first embodiment

of magnetic circuit for a loudspeaker in accordance with the invention;

Fig. 2 is a schematic diagram of a second embodiment of magnetic circuit for a loudspeaker in accordance with the invention; and

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Fig. 3 is a schematic diagram of a third embodiment of magnetic circuit for a loudspeaker in accordance with the invention, here using two voice coils.

Referring first to Fig. 1, there is shown the magnetic circuit of a loudspeaker, the other parts of which are not 10 The assembly comprises a single voice coil 10 which shown. is carried by a former 12 and is positioned within an air gap Two permanent magnets 16a and 16b are positioned 14. adjacent to the air gap 14, one above the voice coil and one 15 below the voice coil. These permanent magnets 16a, 16b can be of a neodymium alloy material for example. The magnetic circuit comprises a plurality of elements of ferromagnetic material, such as mild steel. In this embodiment there are four such elements, which constitute separate pole pieces. 20 These pole pieces are indicated at A, B, C and D. Pole piece A encompasses the permanent magnets and the air gap, while pole pieces B, C and D are positioned to one side of the air gap between the permanent magnets 16a and 16b. One thus has a multi-pole piece structure.

25 The assembly also includes a plurality of rings of conductive material, for example of aluminium or copper. Alternatively, rings of a non-conductive material could be used in some circumstances. Two rings 18a and 18b are positioned on the inside of the air gap 14 and separate the

pole piece elements B, C and D from one another. On the outside of the air gap, directly opposite the rings 18a and 18b are conductive rings 20a and 20b. Adjacent to the bottom of the former 12 are positioned further conductive rings 22 and 24, one on the inside of the former and the other on the outside of the air gap. Adjacent to the top of the former 12 are positioned further conductive rings 26 and 28, the former on the inside of the former 12 and the latter on the outside of the former, in contact with the upper portion of the pole piece element A. An air gap 30 is left between the pole piece elements A and C, and the air gap 14 is enlarged at the bottom of the former around conductive ring 22.

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Referring now to Fig. 2, in which the same or equivalent parts as in Fig. 1 are indicated by the respective same reference numerals, this shows an alternative embodiment, 15 again using air gaps and conductive rings to separate the pole piece elements A, B, C and D from one another. embodiment, the air gap 30 of Fig. 1 is filled by a further ring 32 of conductive material, such as aluminium or copper. 20 Also, the rings 18a and 18b of conductive material in Fig. 1 are here replaced by smaller rings 34a and 34b of conductive material and air gaps 36a and 36b. On the outside of the voice coil the conductive rings 20a and 20b of Fig. 1 are omitted, leaving air gap recesses 38a and 38b opposite the The other elements of the conductive rings 34a and 34b. 25 assembly are unchanged.

Fig. 3 shows an alternative embodiment which comprises two voice coils 40a and 40b, a single permanent magnet 42 and four pole piece plates on each side of the air gap within

The permanent magnet 42 can which the voice coils move. again be of neodymium alloy material and the individual plates of mild steel or other ferromagnetic material. this embodiment the individual plates 44a, 44b, 44c and 44d on the magnet side of the voice coils and the pole piece plates 46a, 46b, 46c and 46d on the outside of the voice coils are each separated by respective air gaps, without the use of conductive rings as in Figs. 1 and 2.

It has been shown that substantial reductions in second harmonic and third harmonic distortion can be achieved with 10 the embodiments of the magnetic circuit shown in Figs. 1 to Taking the embodiment of Fig. 3 as an example, whereas with a conventional magnetic circuit one might achieve a reduction in the second harmonic distortion of -19db, with an 15 accompanying increase in the third harmonic distortion of +3db, with the motor drive of Fig. 3 one can achieve a reduction in the second harmonic distortion of approximately -32db, with a reduction also in the third harmonic distortion of about -5db. One thus has a highly linear motor.

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Although in each of the embodiments described above the pole piece assembly comprises four pole piece elements, it is to be understood that the invention covers also the use of two poles, three poles or more than four poles, with or without rings of conductive or non-conductive material. is only necessary that the three or more poles should be 25 separated or divided in such a way that they are not in direct physical contact one with another and that the magnetic path between the poles should have minimum reluctance.

Although the embodiments described above show magnetic structures which are arranged to provide cylindrical symmetry with respect to an annular air gap, with the symmetry being about the longitudinal axis of the loudspeaker, the invention is also applicable to the use of magnetic circuits which are not axially symmetrical in terms of the magnet geometry. A non-axisymmetric version has higher reluctance between the plates.

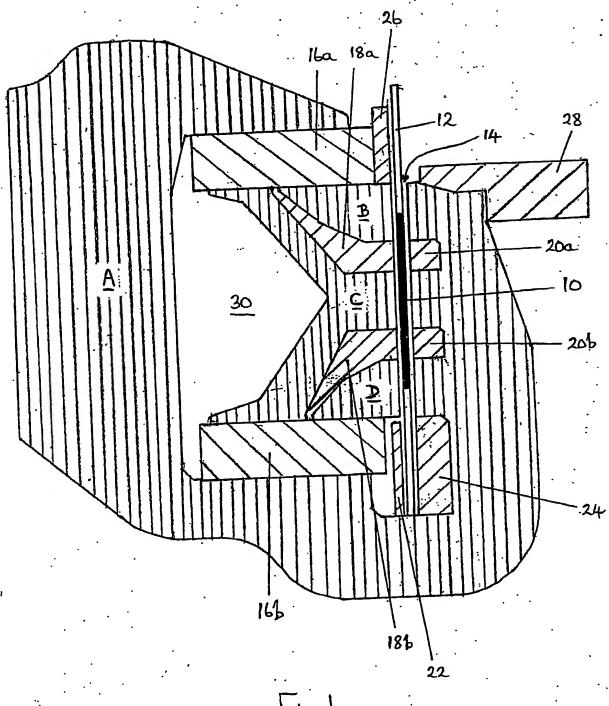


Fig.1.

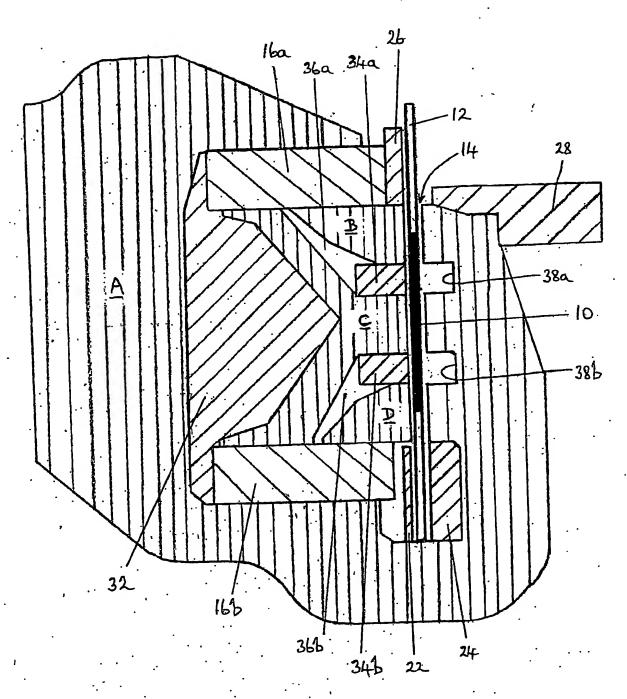


Fig. 2.

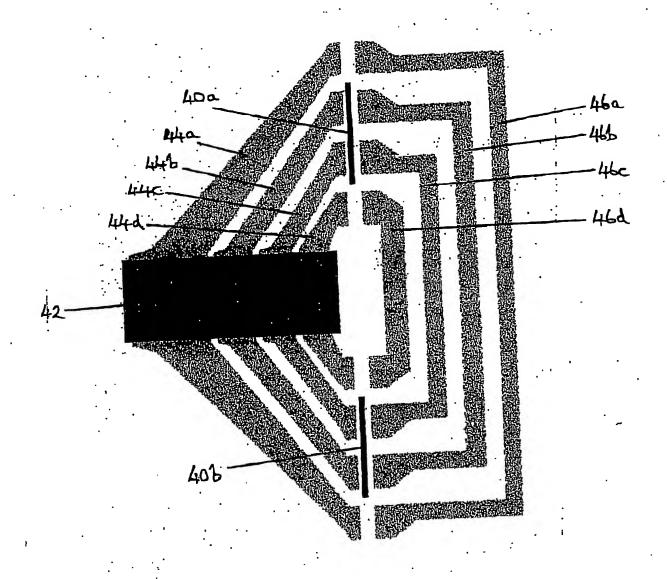


Fig.3